HIGH PERFORMANCE ANTENNA ARRAY FOR 5th GENERATION WIRELESS COMMUNICATION SYSTEMS

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Abstract

In this paper, a probe fed PIFA square array antenna is designed for the fifth generation (5G) wireless applications in EU countries with an allocated frequency band of 24.25GHz - 27.5GHz. The array designed is made up of 16 elements arranged in a 4x4 matrix form, this makes it easily integrated into very portable mobile devices. An impedance bandwidth of 12.5% ranging from 24.25GHz - 27.5GHz was achieved and measured, with each element having a reflection coefficient of less than -15dB and a worse case 14dB mutual coupling. With a uniform amplitude and no inter element phase difference, a maximum broadside gain of about 16.71dB is obtained with an SLL (Side Lobe Level) of 12dB and a 3dB beamwidth of 30 deg. Scanning the main beam to 48 deg in the E-plane (y-z plane) the broadside gain reduces to 14.46dB with a phase difference of 150 deg per column element and an SLL of 6.86dB still maintaining a good beam focus of 30 deg 3dB beamwidth. These good characteristics renders this antenna a good candidate to be deployed for 5G mobile applications.

Contribution/ Originality: This study contributes to the existing literature of works on the design of high performance antenna arrays for millimeter wave 5G frequency bands, having the capability of adaptive beam forming and steering, finding application in mobile and portable devices at a relatively low cost.

1. INTRODUCTION

In modern communication systems the explosive growth in demand for wireless broadband that can carry video and other content-rich services, and the Internet of Things (IoT), where large numbers of smart devices communicate over the Internet has put a high demand on the speed and performance of existing mobile communication network, which has continued to evolve from one generation to another, from 2G(400Mhz - 900Mhz) to 4G(0.9GHz - 2.6 GHz), and currently the development of the 5th Generation wireless systems to achieve these high performance requirements, 5G will provide extreme broadband speed, ultra low latency, and ultra reliable web connectivity [1]. Higher data rates (multi-Gbps) drive the need for greater bandwidth systems, and the available bandwidth in the spectrum up through 6 GHz is not sufficient to satisfy these requirements. (For reference, current cellular operation is below 3 GHz.) This has moved the target operating frequency bands up into the millimeter wave range for the next generation of wireless communication systems. This frequency ranges from 3.3 - 6 GHz and 24 - 39 GHz as specified by the 3rd Generation Partnership Project (3GPP) in Release 15 [2].
This increase in the frequency of communication and the miniaturisation of mobile communication devices antennas has resulted in the high directivity of communication radio waves, in antenna design at high frequencies, it is not practical to make use of omni-directional antennas, due to their low efficiencies and performance at high frequencies, this leads to the need to design highly directional antennas for this application, also signal path and propagation challenges associated with operating at these frequencies also increases. For example, the attenuation due to gas absorption for a 60-GHz waveform is more than 10 dB/km, while a 700-MHz waveform experiences an attenuation on the order of 0.01 dB/km. A problem therefore arises from the use of directional antennas in that the need arises for a device to continuously track the signal path in order to align its main lobe with the direction of arrival of the incoming signal in order to ensure maximum reception and a reliable communication link, while at the same time rejects unwanted signal reception due to interference caused by multipath propagation, which is a prevalent phenomenon at higher frequencies of communication.

To solve this problem phased array antennas \([3]; [4]\) have been developed which adaptively steer the radiating beam direction of the antenna in order to guarantee reliable connectivity and to aid the deployment of 5G mobile communication networking. This work will look into the design and analysis of a phased antenna array suitable for such application.

2. DESIGN OF THE ANTENNA

For the antenna designed in this work, it is intended to be used in mobile devices, given this, it has to meet certain requirements of a mobile device, one of this primary requirement is compactness, an antenna designed to be used in a mobile device has to be compact, this requirement narrows down the choice of our design to the use of microstrip antenna, this is one of the major advantages of a microstrip antenna, apart from this, another reason for the choice of this antenna type is its ease when it comes to complexity of manufacture as well as its cost, also another factor that influenced the use of this antenna type is its relatively low Specific Absorption Rate (SAR), since mobile devices are used in close proximity to the human skin this is of concern.

The specific antenna used in this case is the Planar Inverted F-type Antenna (PIFA) \([3]; [5]\) this antenna is thus chosen also due to its ease in manufacture when it comes to microstrip antennas, because of its simple and less complex nature, an overview of this antenna is shown in the figure below, and also when designed properly, high performance can be achieved from it, and its bandwidth can be as high as 6GHz making this a suitable candidate when designing for an Ultra Wide bandwidth applications.

The antenna in this work is designed to operate in the 26 GHz 5G spectrum bandwidth, 24.25 – 27.5 GHz, this band has been assigned for commercial use in 2020 by the European Union(EU), therefore for the antenna to be designed, the bandwidth expected is 3.25GHz.

The proposed antenna is simulated using Ansys High Frequency Structure Simulator (HFSS), which is a full wave electromagnetic simulation software for the microwave and millimeter wave integrated circuits. Ansoft HFSS employs the Finite Element Method (FEM), adaptive meshing, and brilliant graphics to give an unparalleled performance and insight to all of the 3D EM problems.

3. SINGLE ANTENNA DESIGN

The proposed antenna is a simple rectangular shaped PIFA as shown in Figure 1. The dimensions of the antenna affect properties such as the antenna’s impedance. The feed point and shorting pin point also crucial to affecting the antenna’s impedance as well as it’s gain and radiation pattern. The antenna is fed via a 50 ohms coaxial port. In the design of microstrip antenna a parameter that highly influences its performance is the choice of substrate material used, in the choice of these materials there are trade-offs to be considered between the performance of the material and it cost \([6]\) for this design a standard low cost FR4 epoxy of a relative dielectric constant 4.4 and loss tangent 0.25 is used as the substrate for printed circuit board.
The planar inverted-F antenna (PIFA).


In the design of this antenna the design parameters of concern are derived as given below, some of which such as the frequency of operation, substrate material and height of substrate used are influenced by choice and the need to obtain a good level base performance:

Frequency of operation (f₀): for this design the centre frequency is 26GHz.

Dielectric constant of the substrate (ε_r): For the design of microstrip antennas the required dielectric constant of the material is allowed to have the range 2.2 ≤ ε_r ≤ 12. The dielectric material selected for the design is FR4-epoxy which has a dielectric constant of 4.4. A substrate with a low dielectric constant reduces the dimensions of the antenna and also increases the efficiency of the antenna, this parameter is directly linked with the height of the substrate material. The ones that are most desirable for good antenna performance are thick substrates whose dielectric constant is in the lower end of the range because they provide better efficiency, larger bandwidth, loosely bound fields for radiation into space, but at the expense of larger element size. Thin substrates with higher dielectric constants are desirable for microwave circuitry because they require tightly bound fields to minimize undesired radiation and coupling, and lead to smaller element sizes; however, because of their greater losses, they are less efficient and have relatively smaller bandwidths. Therefore it all results in a compromise between good antenna performance and dimension constraints [7].

Height of the substrate (h): In the design of microstrip antenna given the constraints of compactness, the height of the substrate is given to range from 0.003λ ≤ h ≤ 0.05λ, this parameter directly affects the efficiency of the antenna and its bandwidth so a relatively thick substrate would be ideal, in this design the height is chosen to be 1mm.

Width of the patch (W): For the width of the patch, this is derived using the formula [3]:

\[ W = \frac{v_0}{2 \times f_0} \sqrt{\frac{2}{\varepsilon_r + 1}} \]

From the above formula, \( v_0 = 3 \times 10^8 \times 10^8 \), \( L_c = 26 \times 10^9 \) Hz, \( \varepsilon_r = 4.4 \)

the width of the antenna \( W = 3.51 \)mm.

Length of the patch (L): In the design of a patch antenna a rough approximation of the length is \( \lambda/4 < L < \lambda/2 \). A more accurate procedure to derive of the length L is given thus:

- Determination of the effective dielectric constant of the microstrip using the formula [3]:

\[ \frac{\varepsilon_r}{\varepsilon_r + 1} \]
\[ \xi_{\text{reff}} = \frac{\xi_r + 1}{2} + \frac{\xi_r - 1}{2} \left[ 1 + 12 \frac{h}{W} \right]^{\frac{3}{2}} \]

From the preceding, \( \xi_r = 4.4 \), \( h = 0.5\text{mm} \), \( W = 3.51\text{mm} \).

Therefore the solution \( \xi_{\text{reff}} = 3.52 \xi_{\text{reff}} = 3.52 \).

- Determination of the length extension \( \Delta L \Delta L \)

\[ \Delta L = 0.412h \frac{(\xi_{\text{reff}} + 0.3)(\frac{W}{h} + 0.264)}{(\xi_{\text{reff}} - 0.258)(\frac{W}{h} + 0.8)} \]

Given \( \xi_{\text{reff}} = 3.52 \xi_{\text{reff}} = 3.52 \), \( W = 3.52 \), \( h = 0.5\text{mm} \).

\[ \Delta L = 0.422\text{mm} \]

- Finally we from the length extension the actual length can be calculated using the formula:

\[ L = \frac{v_o}{2 \times f_r \times \sqrt{\xi_{\text{reff}}}} - 2\Delta L \]

Given \( \xi_{\text{reff}} = 3.52 \xi_{\text{reff}} = 3.52 \), \( \Delta L = 0.422\text{mm} \), \( \Delta L = 0.422\text{mm} \),

\[ f_r = 26 \times 10^9 f_{fr} = 26 \times 10^9. \]

The length \( L = 2.5\text{mm} \).

Feed method: In this design the antenna is fed via a coaxial probe. Coaxial-line feeds, where the inner conductor of the coax is attached to the radiation patch while the outer conductor is connected to the ground plane, are also widely used. The coaxial probe feed is also easy to fabricate and match, and it has low spurious radiation. But the down side of this feed method is that it has a narrow bandwidth.

![Figure 2](source: Ansys HFSS)

The Figure 2 shows the proposed antenna, in its perspective view, predominantly showing the antenna patch, also showing the feed pin and shorting pin, as well as the coaxial feed line.
From the above design parameters the antenna was modelled and simulated using ANSYS and the following results were obtained.

For an acceptable performance the return loss parameter $S_{11} \leq -15\, \text{dB}$ . Same goes for the VSWR it is expected that the VSWR $\leq 1.5$.

The Return Loss ($S_{11}$ Parameter) Serves as the Cost, the aim is to adjust the design parameter such that the $S_{11} \leq -15\, \text{dB}$ across the proposed bandwidth of operation, $24.25\, \text{GHz} - 27.5\, \text{GHz}$ this is one of the primary parameters for grading a good antenna.

**Table 1. Dimension parameters of the single antenna element.**

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Values</th>
<th>Parameters</th>
<th>Values</th>
</tr>
</thead>
<tbody>
<tr>
<td>Antenna dimensions</td>
<td></td>
<td>Feed dimensions</td>
<td></td>
</tr>
<tr>
<td>patchX</td>
<td>2.7mm</td>
<td>feedX</td>
<td>1mm</td>
</tr>
<tr>
<td>patchY</td>
<td>1.2mm</td>
<td>feedY</td>
<td>0.1mm</td>
</tr>
<tr>
<td>Shorting pin</td>
<td></td>
<td>coax_inner_radius</td>
<td>0.06mm</td>
</tr>
<tr>
<td>dimensions</td>
<td></td>
<td>shortX</td>
<td>-1.2mm</td>
</tr>
<tr>
<td></td>
<td></td>
<td>coax_inner_radius</td>
<td>0.51mm</td>
</tr>
<tr>
<td></td>
<td></td>
<td>shortY</td>
<td>-0.3mm</td>
</tr>
<tr>
<td></td>
<td></td>
<td>feedLength</td>
<td>1.7mm</td>
</tr>
<tr>
<td>pin_radius</td>
<td>0.03mm</td>
<td>Design frequency</td>
<td>26GHz</td>
</tr>
<tr>
<td>Substrate dimensions</td>
<td></td>
<td>gnd_x</td>
<td></td>
</tr>
<tr>
<td>subH</td>
<td>1.5mm</td>
<td>gnd_y</td>
<td>subY</td>
</tr>
<tr>
<td>subX</td>
<td>6mm</td>
<td></td>
<td></td>
</tr>
<tr>
<td>subY</td>
<td>6mm</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

The above parameters are the obtained final parameters that resulted in obtaining the stated optimum operating requirements of the antenna element. The optimization was performed using Quasi Newton (Gradient) optimization, in the optimization the return loss $S_{11}$ set as the cost function with the aim of obtaining a value $S_{11} \leq -15\, \text{dB}$. This goal was attained and will be discussed.

4. SINGLE ANTENNA ELEMENT ANALYSIS

From the optimization, the results and plots obtained from the optimized parameters antenna are given,

Figure 3a shows the 3D far field plot of the antenna at its centre frequency 26GHz, (b) shows the elevation polar plot at phi = 0 deg H-plane (x-z plane (red)) and at phi = 90 deg E-plane (y-z plane (purple)).
Figure 4. (a) Return Loss (S11 parameter) (b) Gain Plot (dB).

From the above plots the optimized antenna has performed has good characteristics as intended in its design bandwidth.

Figure 4a shows the return loss plot (S11 parameter) as seen from the diagram, the return loss of the antenna is impressive over it operating bandwidth a return loss of less than -15dB was obtained, in fact in effect the operating bandwidth of the antenna is 29.38 GHz - 22.75GHz, this gives an impressive bandwidth of 6.6GHz, shows that the antenna is a good choice for 5G wireless network systems.

Figure 4b shows the peak gain of the antenna in its boresight direction, a maximum gain of 5.43dB is attained at 26 GHz, this includes an average gain of 5.3dB shows high performance.
Figure 5 shows the VSWR of the antenna, this value aids in evaluating the level of mismatch between the antenna and its feed network, from the above, a low VSWR of less than 1.5 was obtained. This shows a good match between the antenna and its feed network, which means a low loss value or reflection coefficient as shown earlier in the $S_{11}$ parameter plot, in Figure 4a.

Source: Ansys HFSS.
Figure 6a shows the plot of the antenna's efficiency over its operating frequency, it has an average radiating efficiency of 89.2%, peaking out at its centre frequency 26GHz at 89.6%, this is shows high performance, ie the antenna is able to convert 89% of received electrical power at its power into radio waves.

Figure 6b shows the elevation plot of the antenna over the elevation angle theta (H-plane), this shows its half power (3dB) beamwidth of 50deg.

5. ANTENNA ARRAY DESIGN

In the configuration of this antenna design a 4x4 array is implemented. The 16 element antenna array is of length 41.08 mm × 41.08 mm. A standard low cost FR4 epoxy of a relative dielectric constant 4.4 and loss tangent 0.25 is used as the substrate for printed circuit board of size 41.08 mm × 41.08 mm. The antenna array is spawn from the above single element design a simple rectangular PIFA (planar inverted-F antenna). The antenna is designed to be integrated into the chassis of a mobile device.

The proposed antenna is arranged as a 4x4 element array with a separation of 5.7mm in both the x and y direction between each element to ensure good isolation between the antenna elements and minimize the grating lobes. The antenna array covers a frequency range of 24.25-27.5 GHz with a bandwidth of 3.25 GHz.

The proposed antenna array design is shown in Figure 7.

| Table 2. Dimension parameter for the antenna array. |
|---------------------------------|-----------|
| Parameters                      | Value     |
| Patch dimensions                |           |
| Inter patch_spacing (x,y)       | 5.7mm     |

6. ANTENNA ARRAY ANALYSIS

The radiation efficiency of the antenna array is shown in Figure 8a the antenna array was able to achieve a peak efficiency of 84.7% at 24.25GHz and an average efficiency of about 83.06% over its operating bandwidth 24.25GHz - 27.5GHz.
The gain of the antenna array is shown in Figure 8b from this plot, the antenna was able to achieve a maximum gain of about 16.71dBi and an average gain of 16.1dB.
For the beam steering, the alternate excitation phase difference between each column element, is varied with so that the direction of the main beam is being stirred in the E-plane. Table 3 below shows the variation of this phase such that the beam is steered at an angle of 48 deg in the E-plane while maintaining an SLL difference value of about 6.86dB, the diagram for the radiation pattern at maximum scan angle is shown in Figure 9.

![E-plane Radiation Gain (phi = 90deg)](image)

**Figure 9.** Radiation pattern for maximum scan angle.

Table 3 gives the radiation characteristics, this shows information about the radiation when there is no phase difference ie dhpi = 0deg, and when the amplitude is the same, in this state of excitation, the boresight beam is 0 deg to with respect to the E-plane and a maximum gain of 16.71dB is achieved in this direction and an SLL of 12dB. Also at maximum scan, the phase difference between each element along the column wise elements dhpi = 150deg, this causes the main beam to stir to an angle of about 48 deg along the E-plane, a gain of 14.46dB is achieved and an SLL of 6.86dB. In each state a steady 3dB beamwidth of 30deg was maintained across the scan.

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Beam position</th>
<th>Max gain</th>
<th>3dB-beamwidth</th>
<th>SLL</th>
<th>DHPI</th>
</tr>
</thead>
<tbody>
<tr>
<td>Boresight</td>
<td>0 deg</td>
<td>16.71dB</td>
<td>30 deg</td>
<td>12 dB</td>
<td>0 deg</td>
</tr>
<tr>
<td>Maximum scan</td>
<td>48 deg</td>
<td>14.46 dB</td>
<td>30 deg</td>
<td>6.86 dB</td>
<td>150 deg</td>
</tr>
</tbody>
</table>

Source: Ansys HFSS.

In order to have a perspective of the performance of the antenna designed in this work it is compared with other works as shown in Table 4.

**Table 4.** Comparison with other reported works on millimeter wave antenna array for 5G applications.

<table>
<thead>
<tr>
<th>Works</th>
<th>Imp. bandwidth</th>
<th>Gain</th>
<th>Rad. efficiency</th>
<th>SLL</th>
<th>Scan range</th>
<th>3-dB beamwidth</th>
</tr>
</thead>
<tbody>
<tr>
<td>Stanley, et al. [8]</td>
<td>6 GHz</td>
<td>13 dBi</td>
<td>7.5%</td>
<td>-</td>
<td>120 deg</td>
<td>-</td>
</tr>
<tr>
<td>This work</td>
<td>6 GHz</td>
<td>16.71 dBi</td>
<td>84.7%</td>
<td>-12 dB</td>
<td>96 deg</td>
<td>30 deg</td>
</tr>
</tbody>
</table>
7. CONCLUSION

In this work, a novel low cost PIFA antenna has been designed and analysed and is seen to be suitable to deployed in 5G mm-wave mobile devices, due to its compactness, and performance, the antenna performed recommendable over its operating bandwidth of 3.25GHz from 24.25GHz - 27.5GHz, with a low return loss ($S_{11} < -15$dB), it also achieved a gain of 5.43dB in its boresight direction. This single antenna element was then scale into a 16 element array of 4x4 configuration, achieving a high gain of 16.71 dB at zero scan angle and a gain of 14.46dB at 48 deg scan angle.

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